

Cellulose Reinforced High Density Polyethylene

Presented by

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M.S. Thesis Defense

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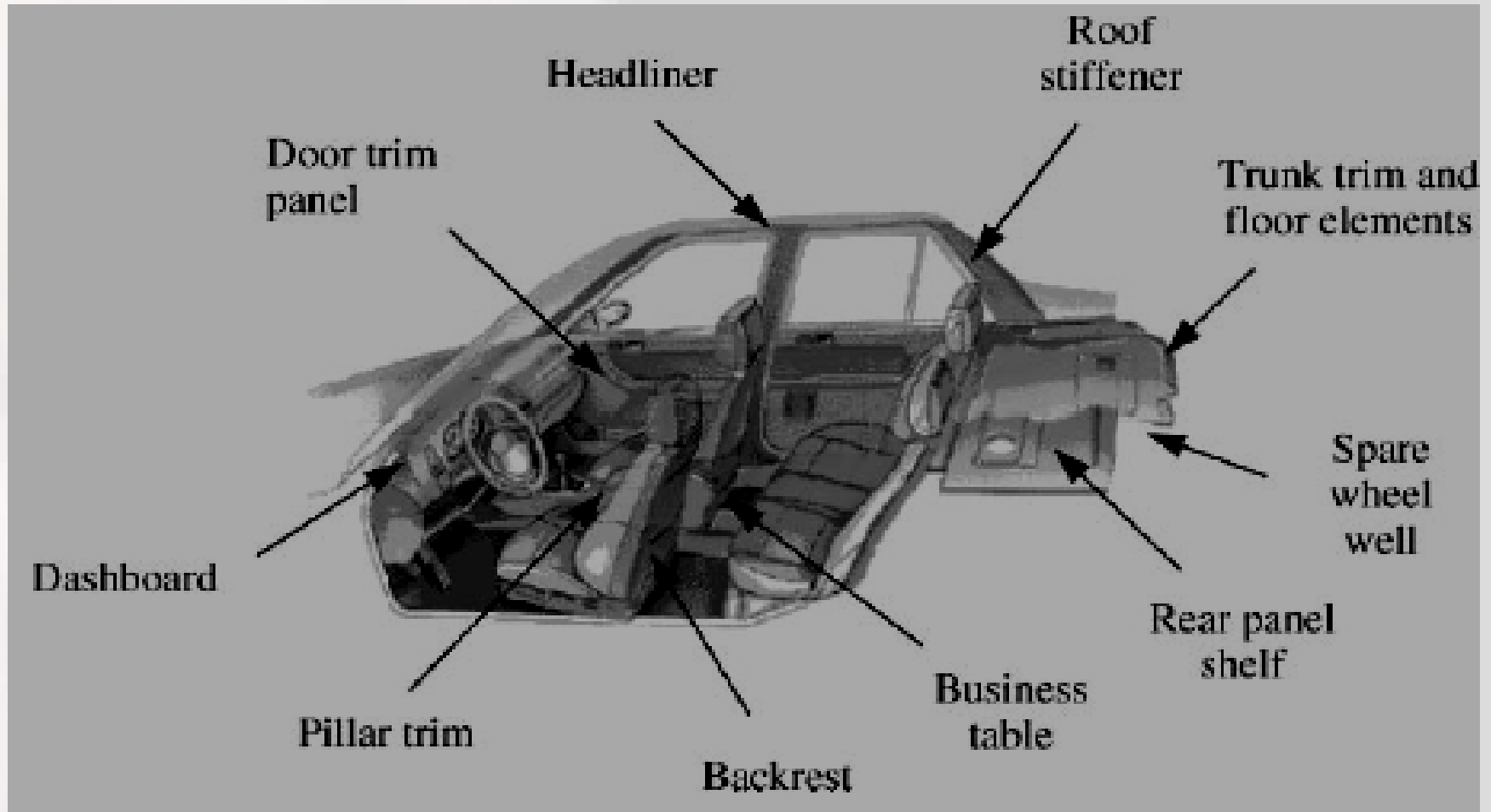
Dr. Ralph Busch

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Background

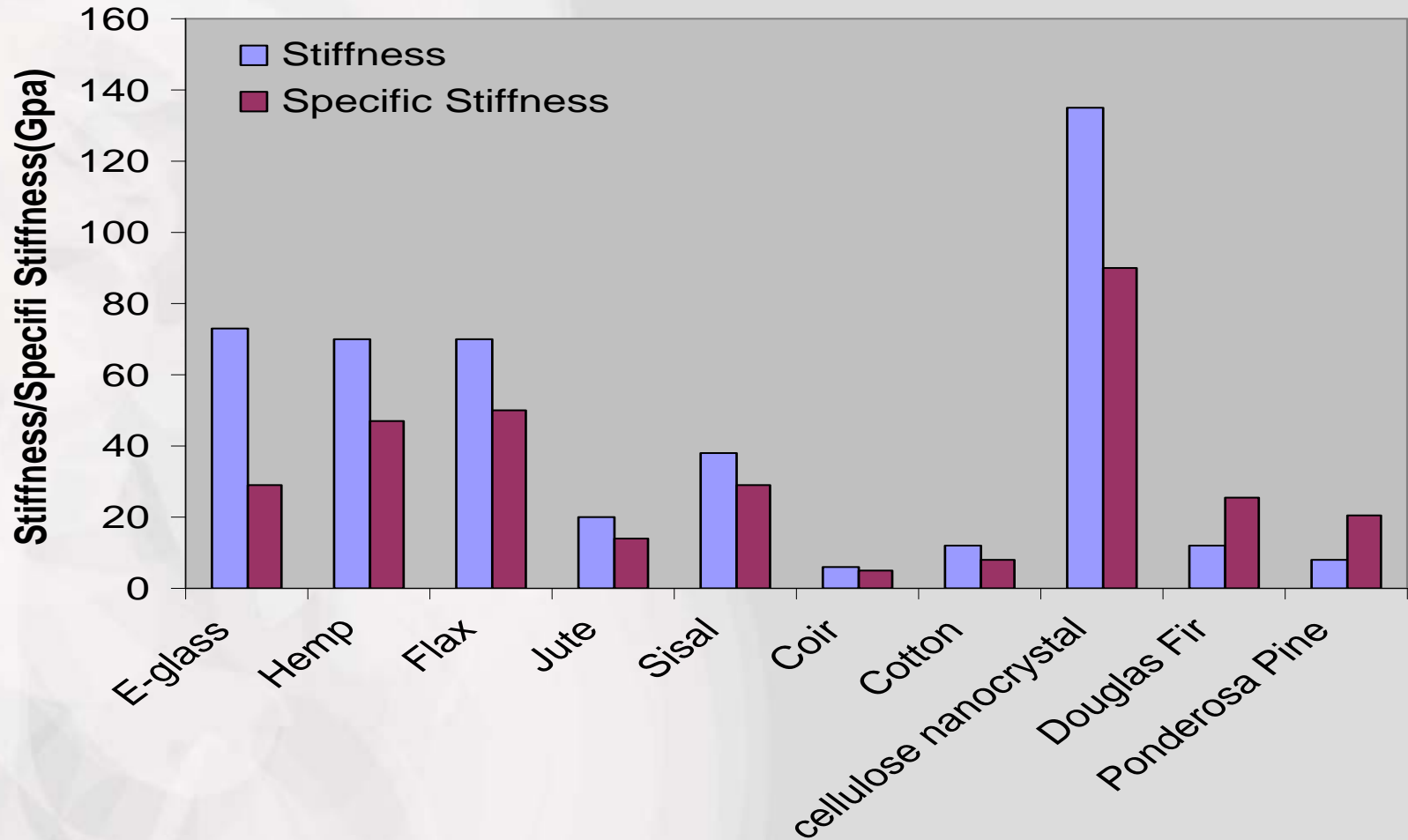
Natural Fiber Reinforced Composites (NFRP) applications in Car Interiors



Some More Applications

- ⊕ **Heat deflection temperature**
- ⊕ **Gas barrier / permeability**
 - ◆ **Packaging materials**
- ⊕ **Electrical conductivity**
 - ◆ **Electronics ,Housing appliances**
- ⊕ **Flame retardancy**

Property Comparison Among the Commonly Used Reinforced Fibers



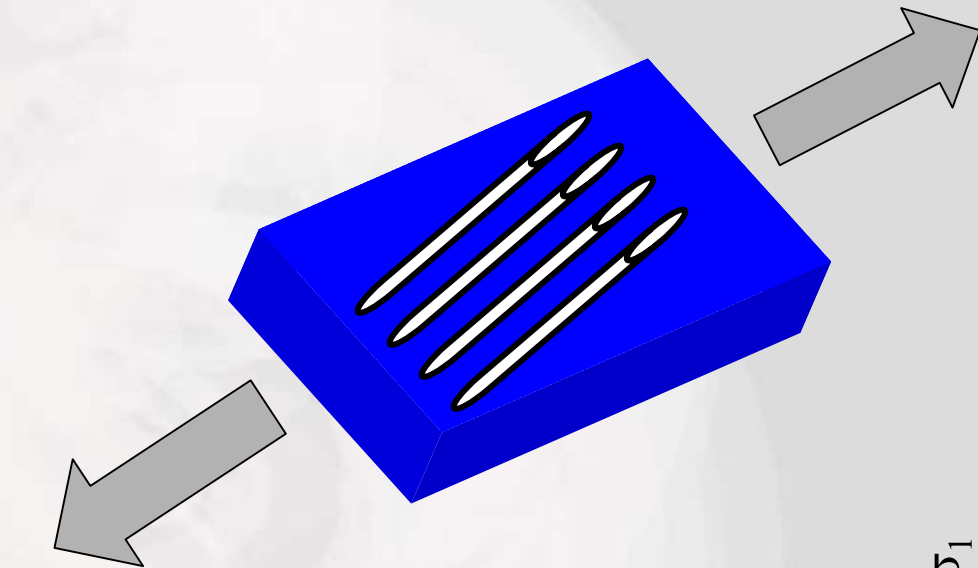
Introduction

⊕ Why cellulose-reinforced thermoplastics?

- ◆ Property enhancement at lower density and cost than synthetic fiber materials (glass, carbon)
- ◆ Non-abrasive and easily recyclable compared to inorganic fillers
- ◆ High strength to weight ratio
- ◆ Sound abatement capability
- ◆ Low energy for processing

(6500 BTU/lb of kenaf ; 23,500BTU/lb of glass fiber)

Role of fiber and Matrix in FRP

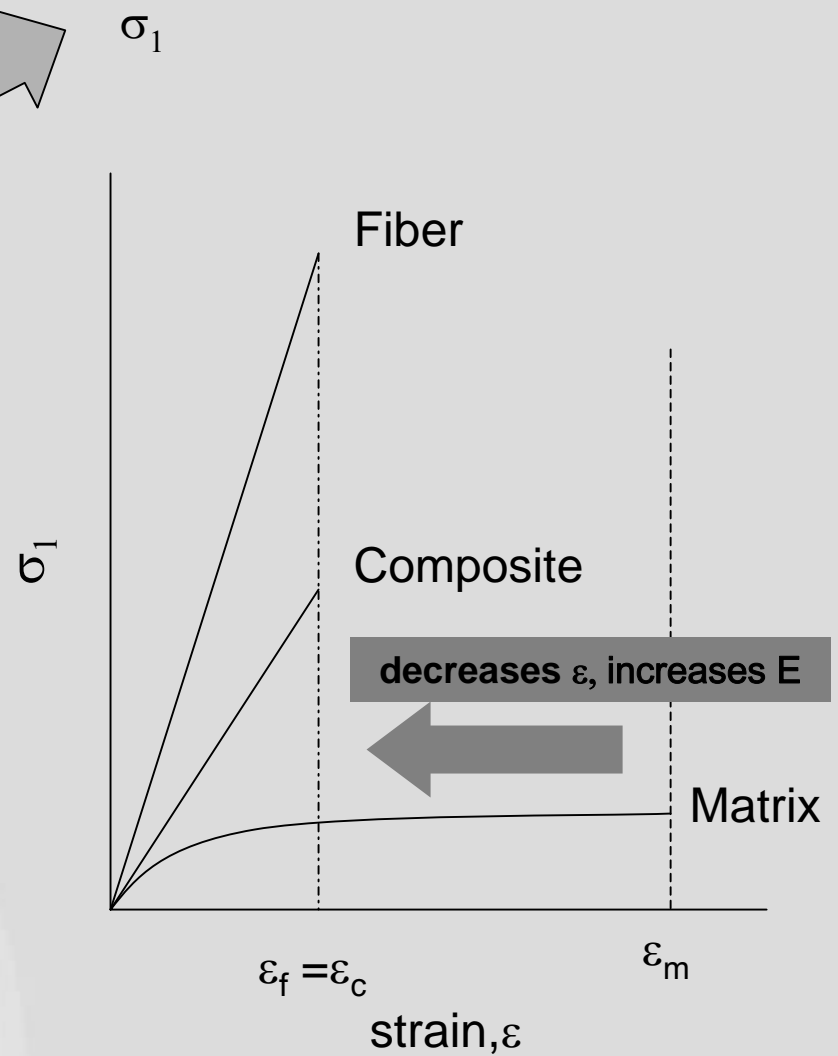


σ_1
⊕ **Fiber**

- ◆ High stiffness
- ◆ Brittle

⊕ **Matrix**

- ◆ Medium for stress transfer
- ◆ Binds the fiber together

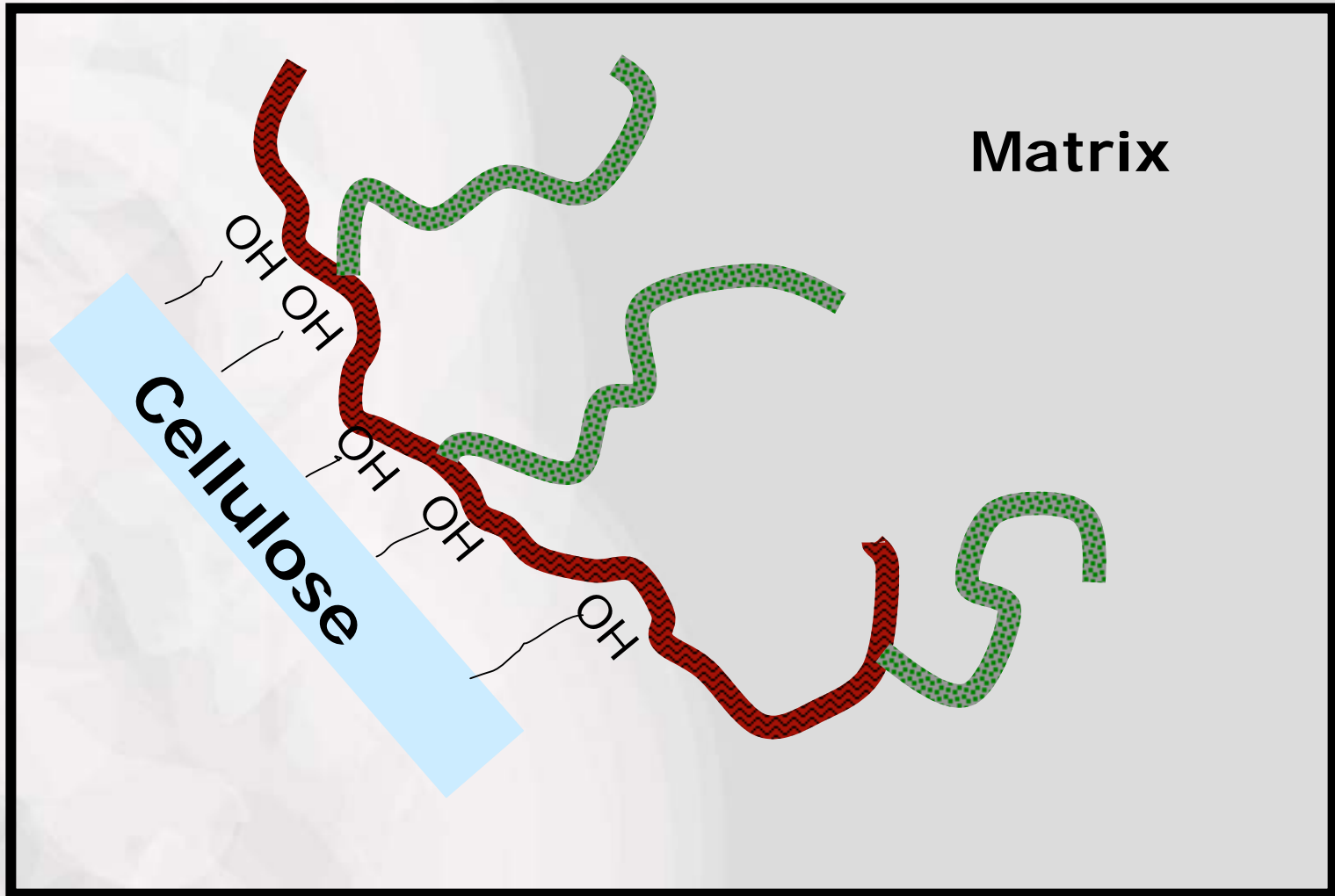


Stress-Strain curve

Fiber Reinforced Composite - Issues

- ⊕ Fiber dispersion
 - ◆ Dispersing agent
- ⊕ Interfacial adhesion
 - ◆ **Compatibilizer or coupling agents**
 - ◆ Surface modification of fibers
- ⊕ **Effect of filler on the crystallization behavior of polymer**

Compatibilizer – Function and Mechanism



Objectives

- ⊕ To prepare nanocrystalline cellulose with high aspect ratio
- ⊕ To investigate the material properties of nanocrystalline cellulose (NCC) filled high density polyethylene (HDPE)
- ⊕ To use microcrystalline cellulose (MCC) as a model filler for NCC
- ⊕ To disperse MCC using a coupling agent system
- ⊕ To study the non-isothermal crystallization kinetics of the filled composites

Materials

⊕ **Matrix: High Density Polyethylene**

⊕ **Filler**

- ◆ **Cellulose nanocrystal from Cotton**

- ◆ **Microcrystalline cellulose (FMC Corp, NJ)**

⊕ **Coupling agent:**

- ◆ **MAPE (Optipak 210)**

- ◆ **Developed by Kaichang Li's lab**

- ◆ **AKD (Aquapel 364)**

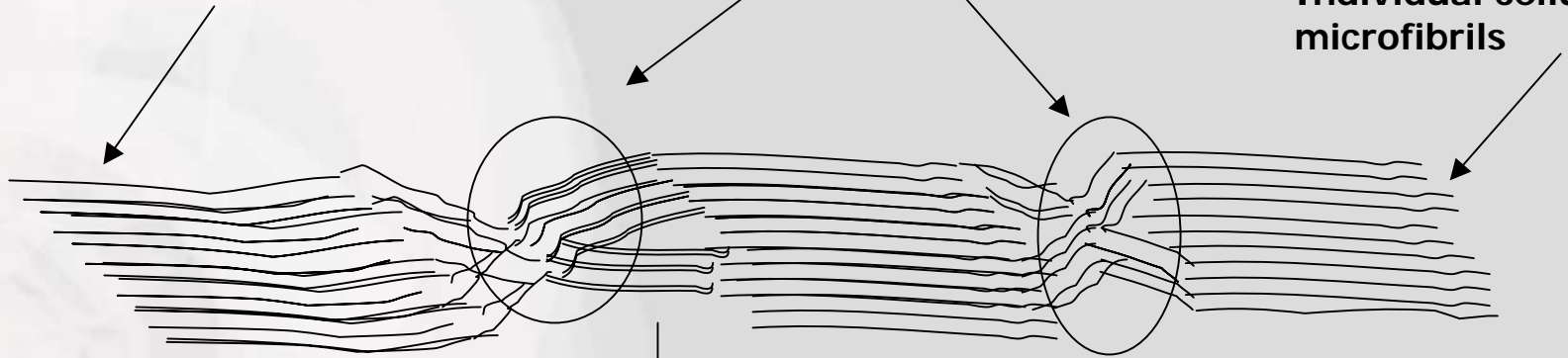
- ◆ **PMDI (Rubinate 1840)**

Experimental Methods

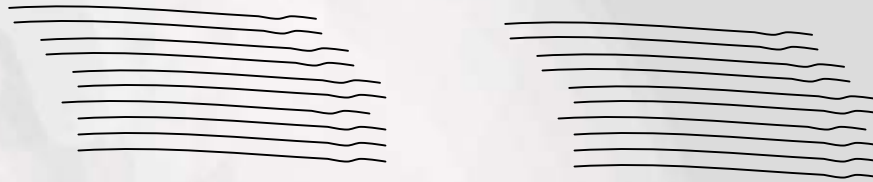
Crystalline regions

Amorphous region

Individual cellulose microfibrils



Acid hydrolysis



Individual crystallites

Schematic of acid hydrolysis of cellulose

Composite Preparation Method

⊕ Brabender Plasticorder

- ◆ Melt mixing HDPE and NCC/MCC at 180 °C for 10 min
- ◆ MAPE (0.4 wt%) and AKD-PMDI (1.0 wt%) was added during mixing

⊕ Carver Hot press

- ◆ Compression molding at 185 °C at 348.5 kPa for 10 min

Composite Characterization Techniques

⊕ Mechanical testing –Sintech 1G, Universal testing machine

- ◆ Flexural strength (MOR) and Flexural modulus (MOE) were measured according to ASTM D 790-02

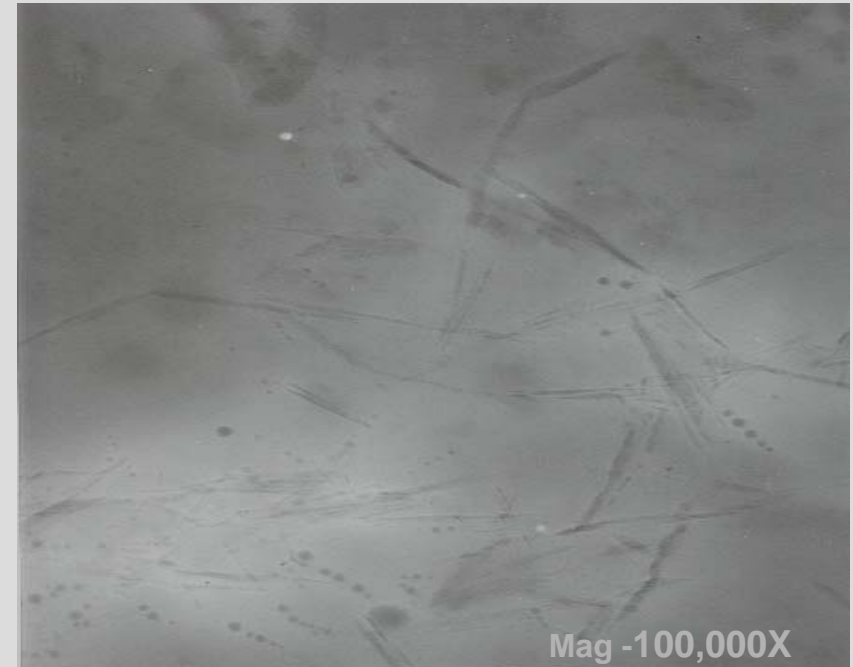
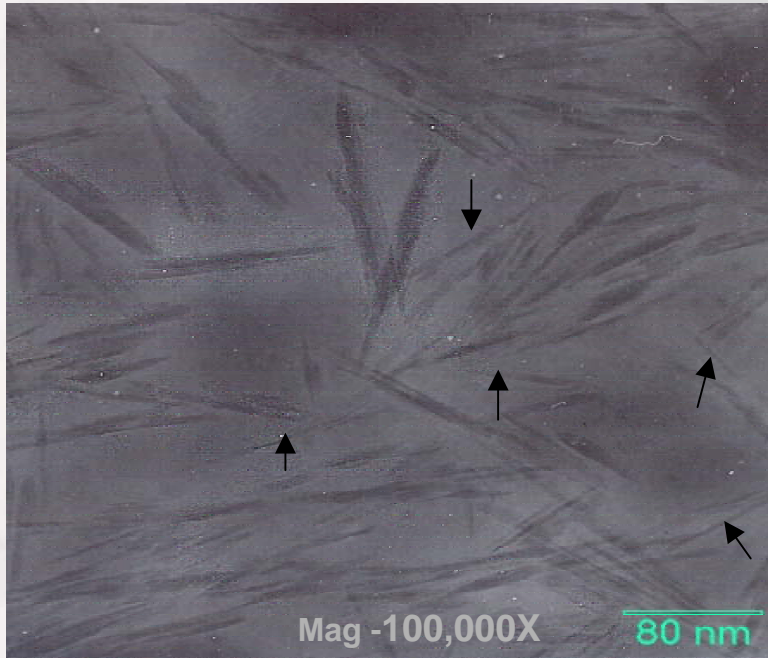
⊕ Thermal Analysis

- ◆ Differential Scanning Calorimetry, TA Instruments DSC 2920
 - Temperature range – 20-200°C
 - Heating/cooling rate – 5, 10, 12.5, 15°C/min
- ◆ Thermo gravimetric analysis , TA Instruments, Q500
 - Temperature range – 40-600°C
 - Heating rate –10°C/min

Results – TEM Characterization/ Mechanical Testing



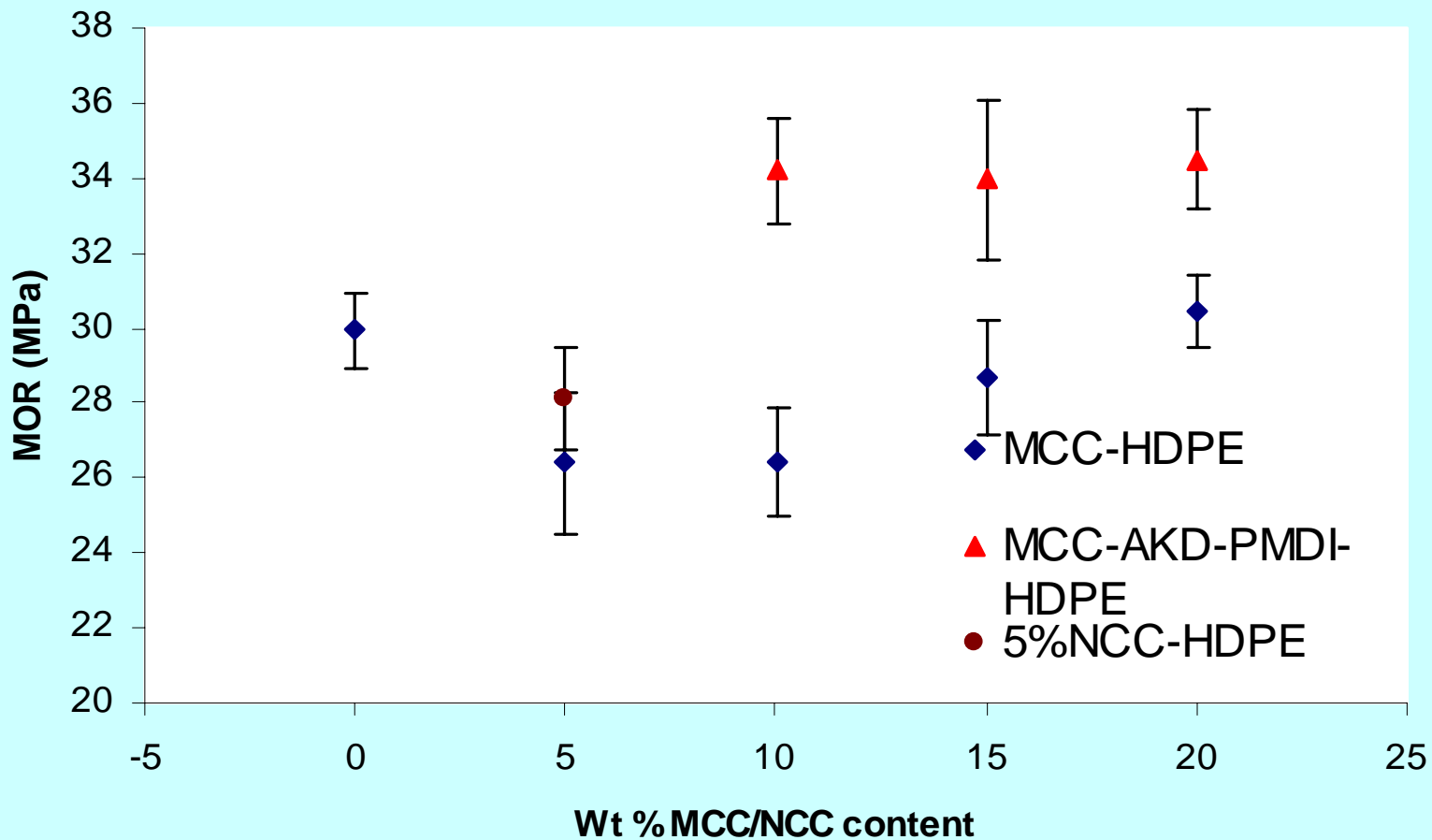
Transmission Electron Micrograph From Cellulose Nanocrystal Suspension Negatively Stained With Ammonium Molybdate



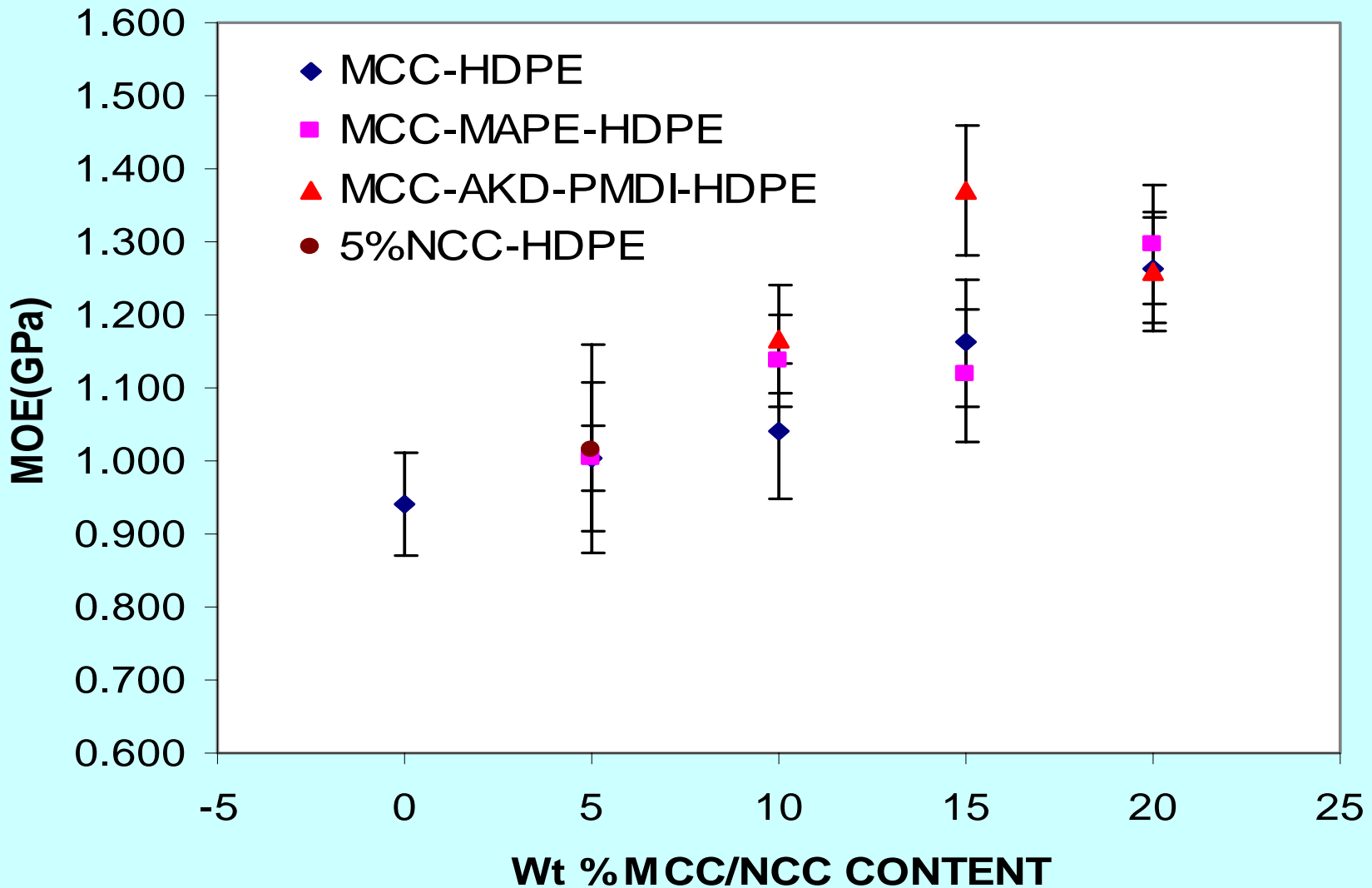
Aspect ratio = L/d

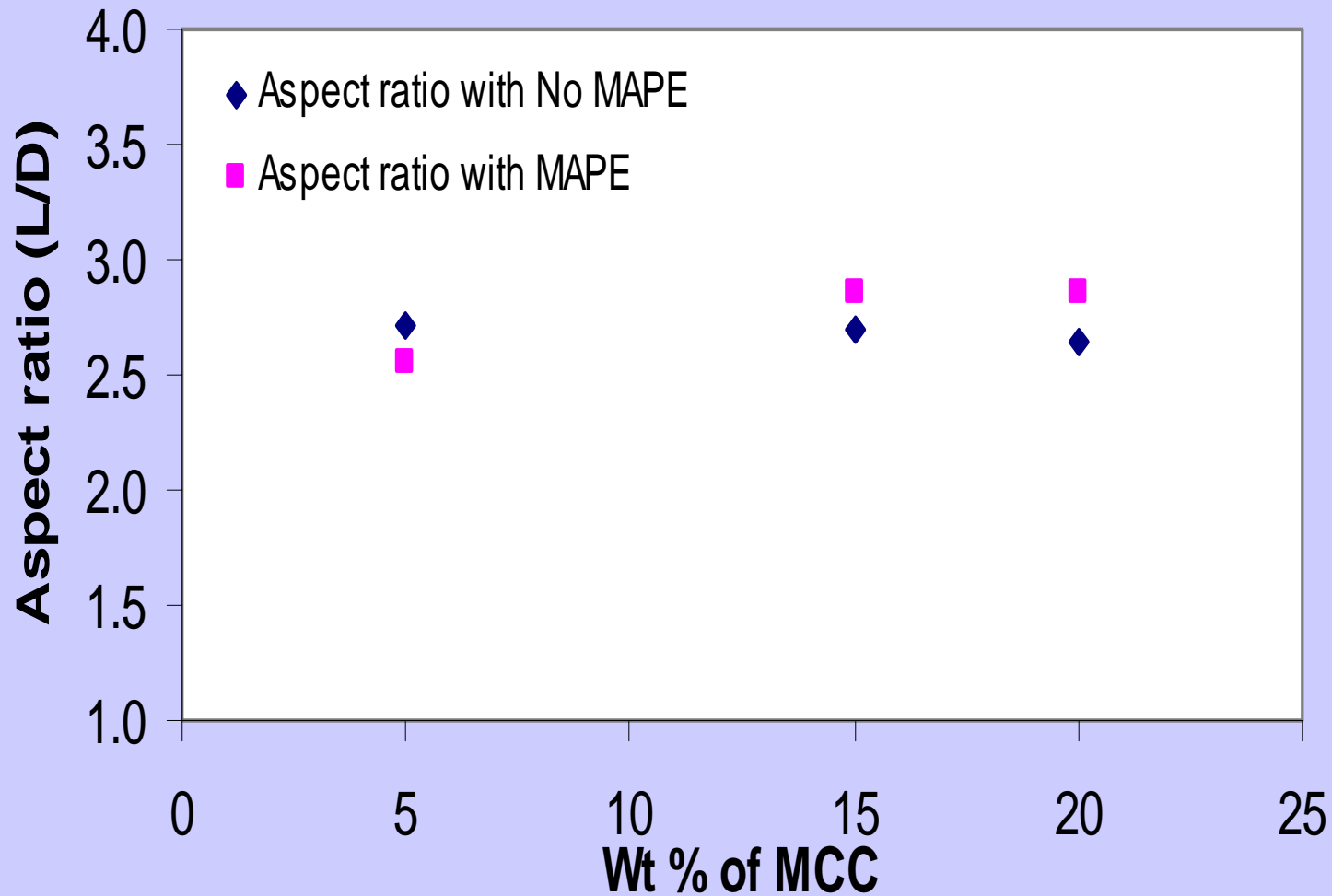
- ⊕ Diameter – 4nm
- ⊕ Length – 120 – 160 nm
- ⊕ Aspect ratio – 30-40

Flexural Strength (MOR)



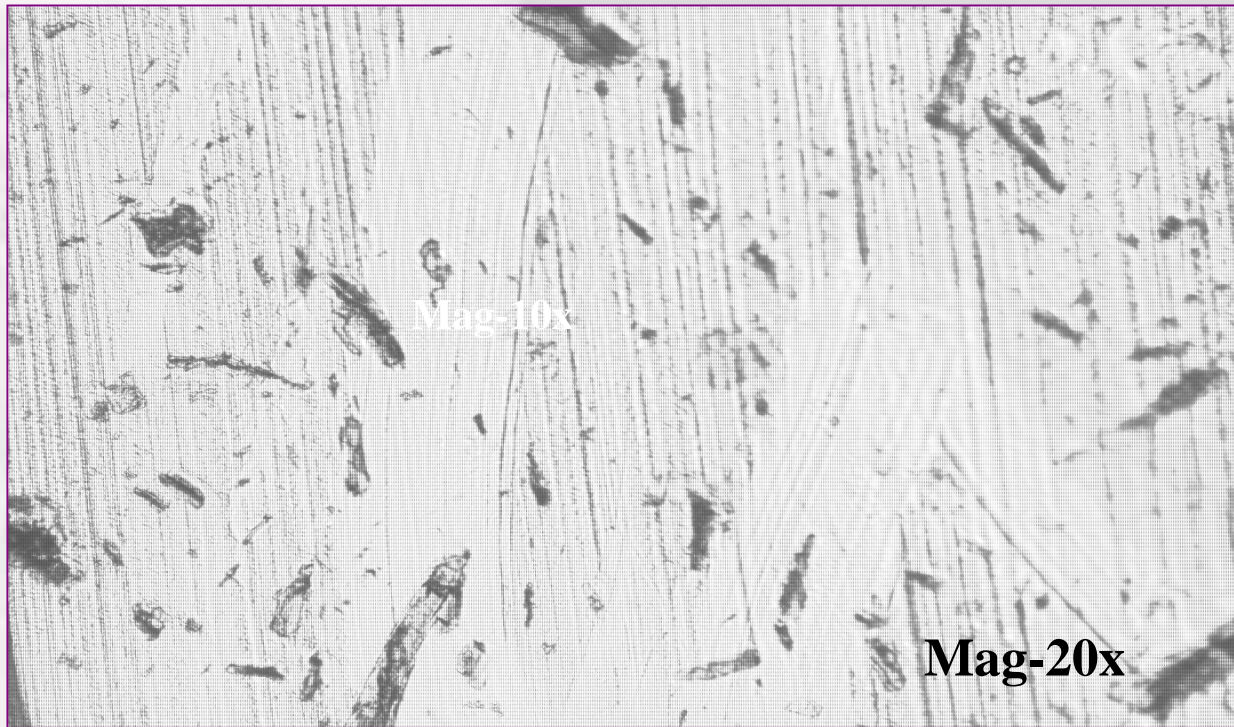
Flexural Stiffness





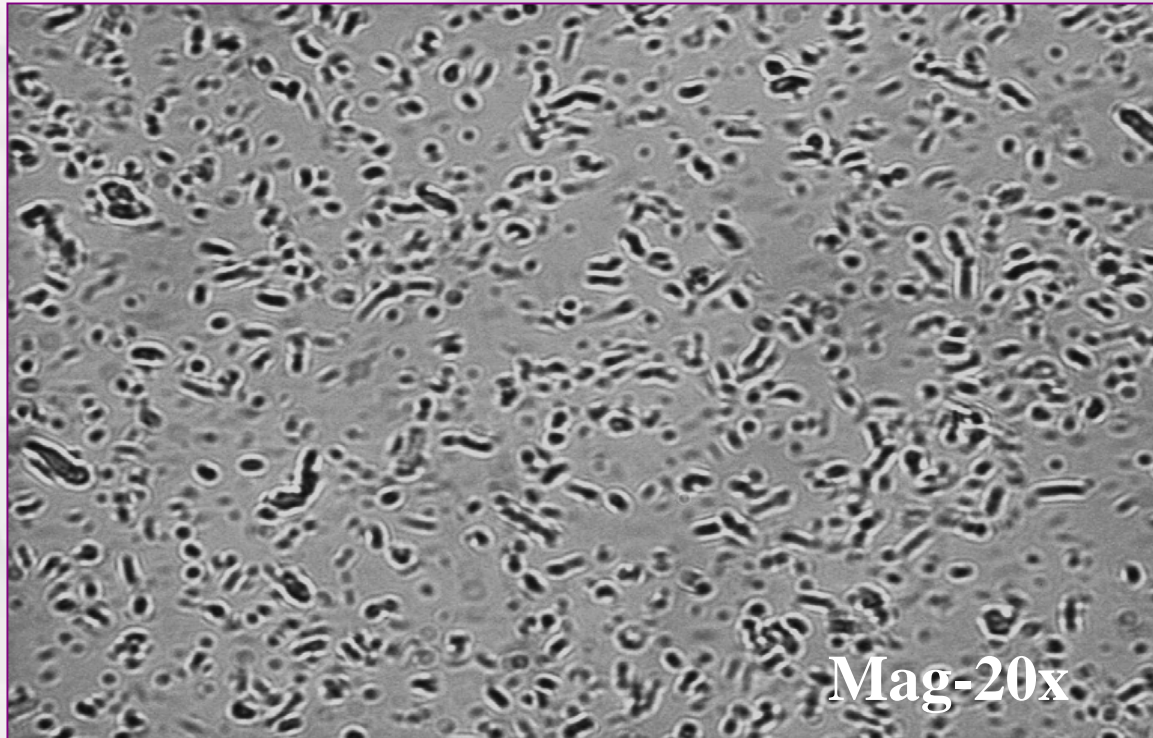
⊕ Low aspect ratio due to agglomeration

Light Microscopy Image of the Cross Section Perpendicular to the Length of the Samples



**Agglomerated cellulose fibers in
5%NCC-HDPE composite**

Light Microscopy Image of the Cross Section Perpendicular to the Length of the Samples



**Dispersed cellulose fibers in 5%MCC-AKD—
PMDI-HDPE sample**

THERMAL ANALYSIS

**Differential Scanning Calorimetry/
Thermal Gravimetric Analysis**



Polymer Crystallization

⊕ Isothermal Crystallization

- ◆ Constant temperature process
- ◆ Avrami, Ozawa, Kissinger

⊕ Non- Isothermal crystallization

- ◆ Constant cooling rate process
- ◆ Simulates real processing conditions
- ◆ Modified Avrami, Kissinger

Kissinger Method – Activation Energy (E_a)

$$d (\ln \phi/T_p^2) /d(1/T_p) = -\Delta E/R$$

ϕ – Cooling rate ($^{\circ}\text{k}/\text{min}$)

T_p – Crystallization peak temperature (k)

ΔE – Activation energy (kJ/mole)

R- Universal gas constant (= 8.314 j/mol k)

Melting

$$\text{Matrix Crystallinity} = \frac{\Delta H_c}{\Delta H^0_c}$$

Heating

Endothermic

Exothermic

dQ/dT

Low temp

High temp

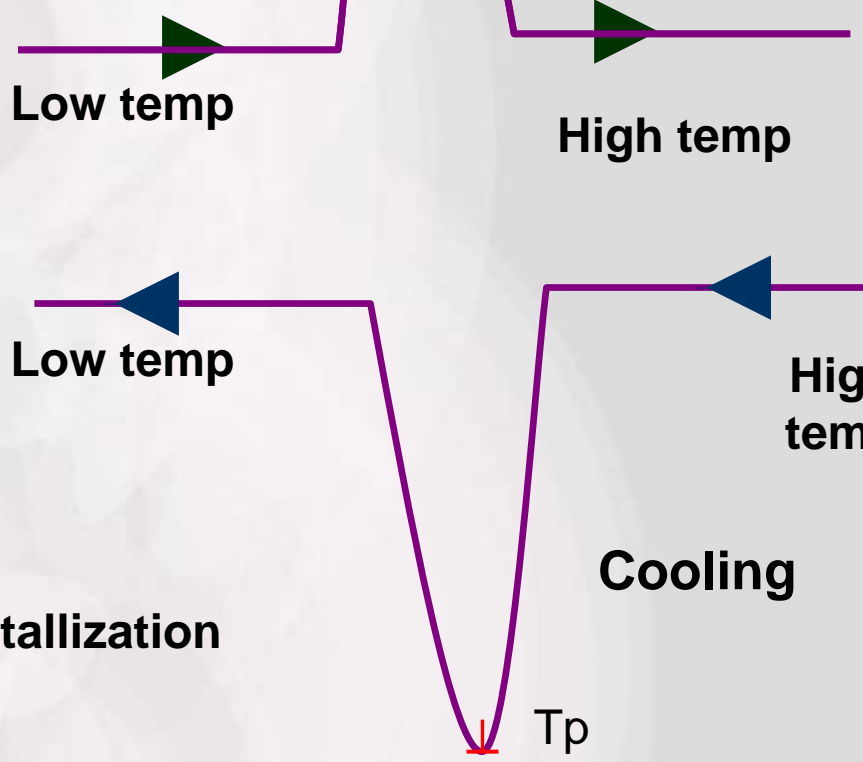
Low temp

High temp

Cooling

Crystallization

Tp



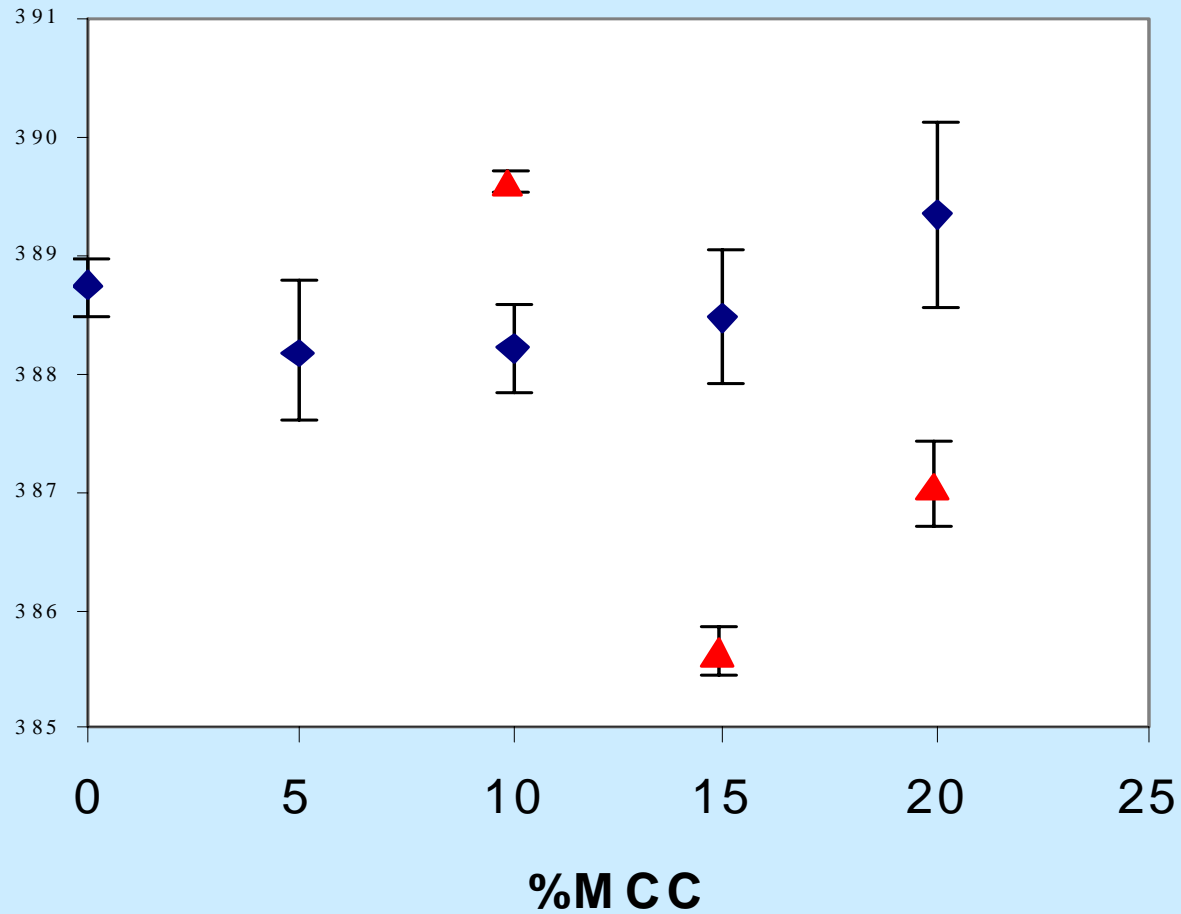
RESULTS

Thermal Analysis

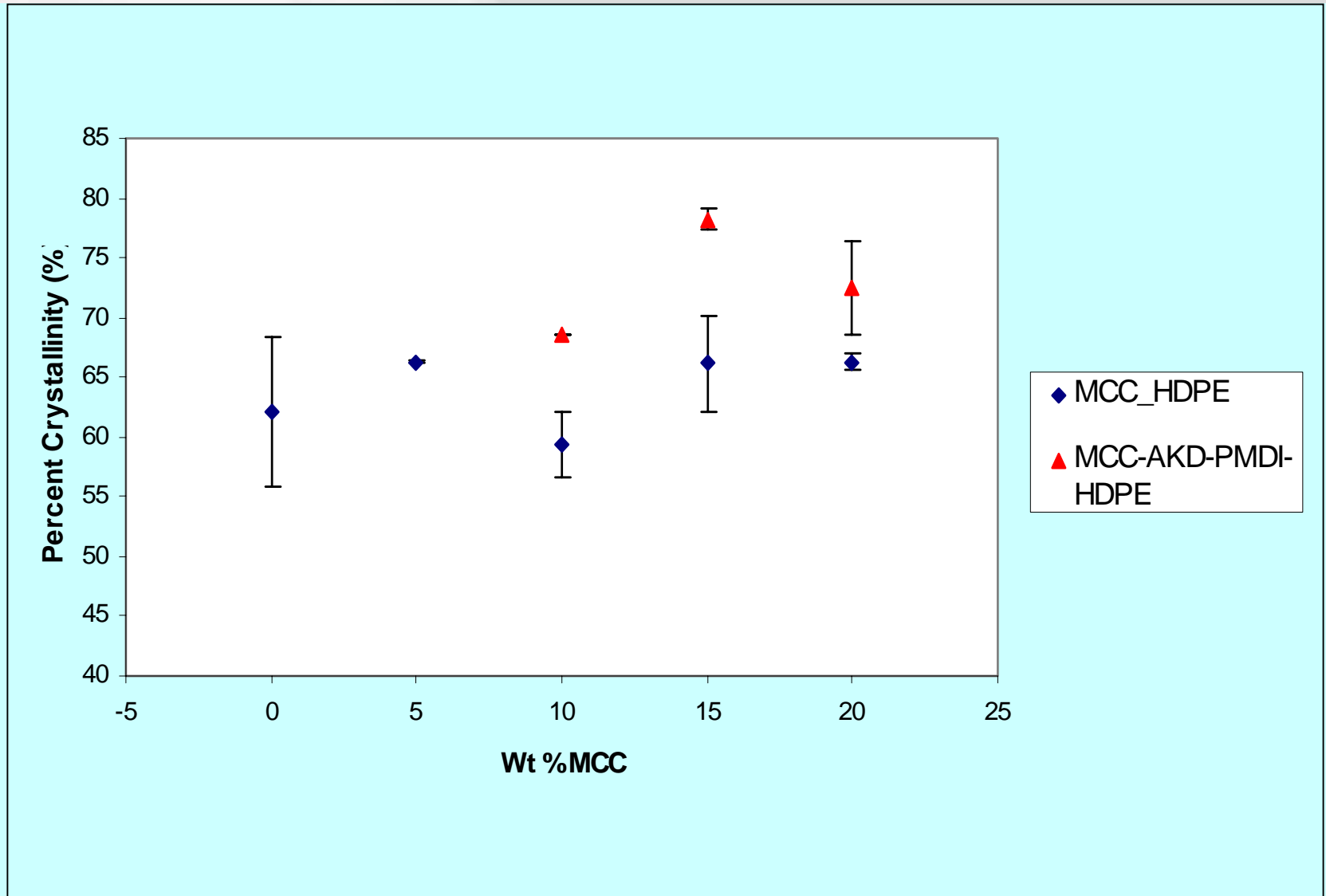


Crystallization Peak Temperature

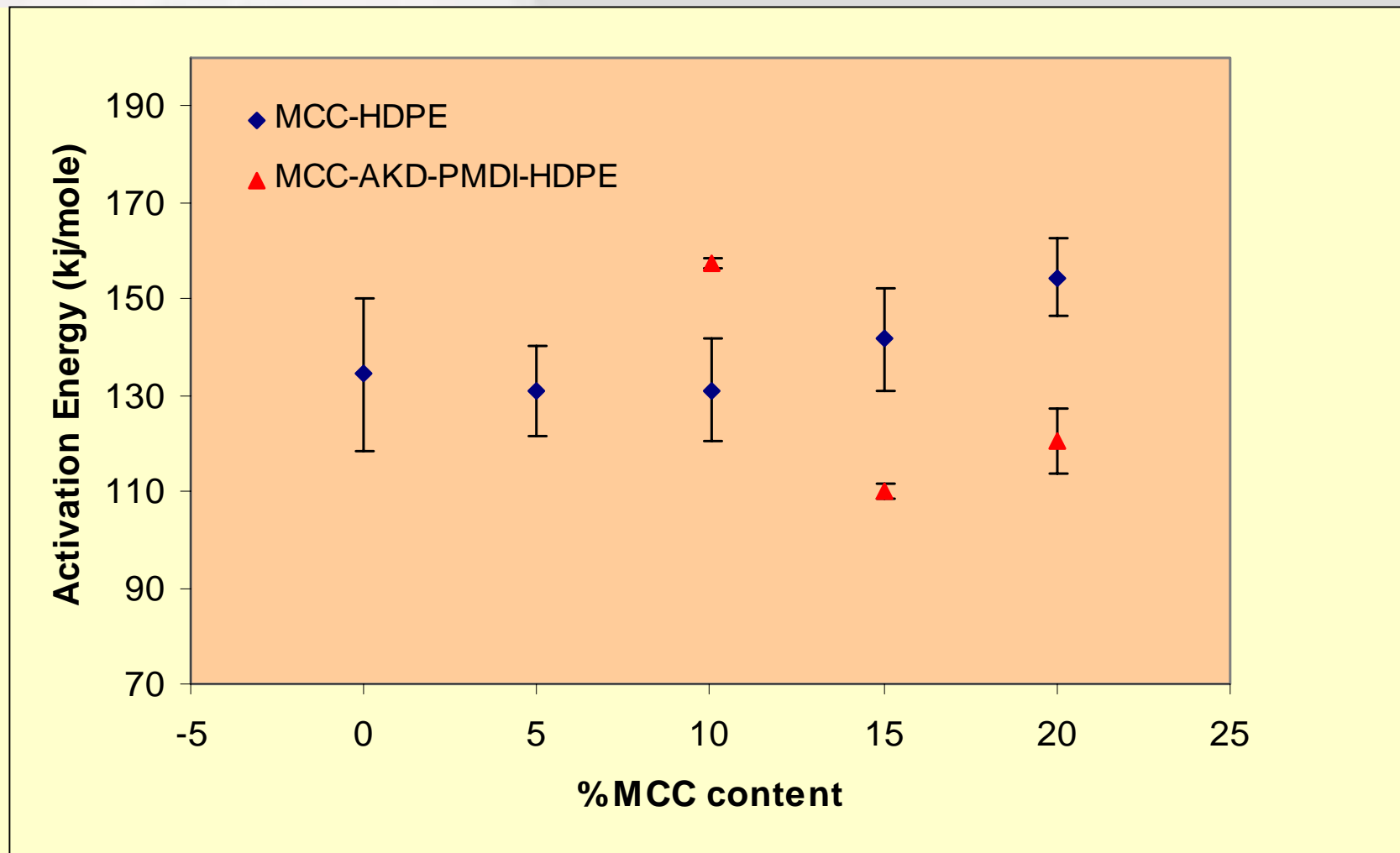
Crystallization peak temperature at 10 per min



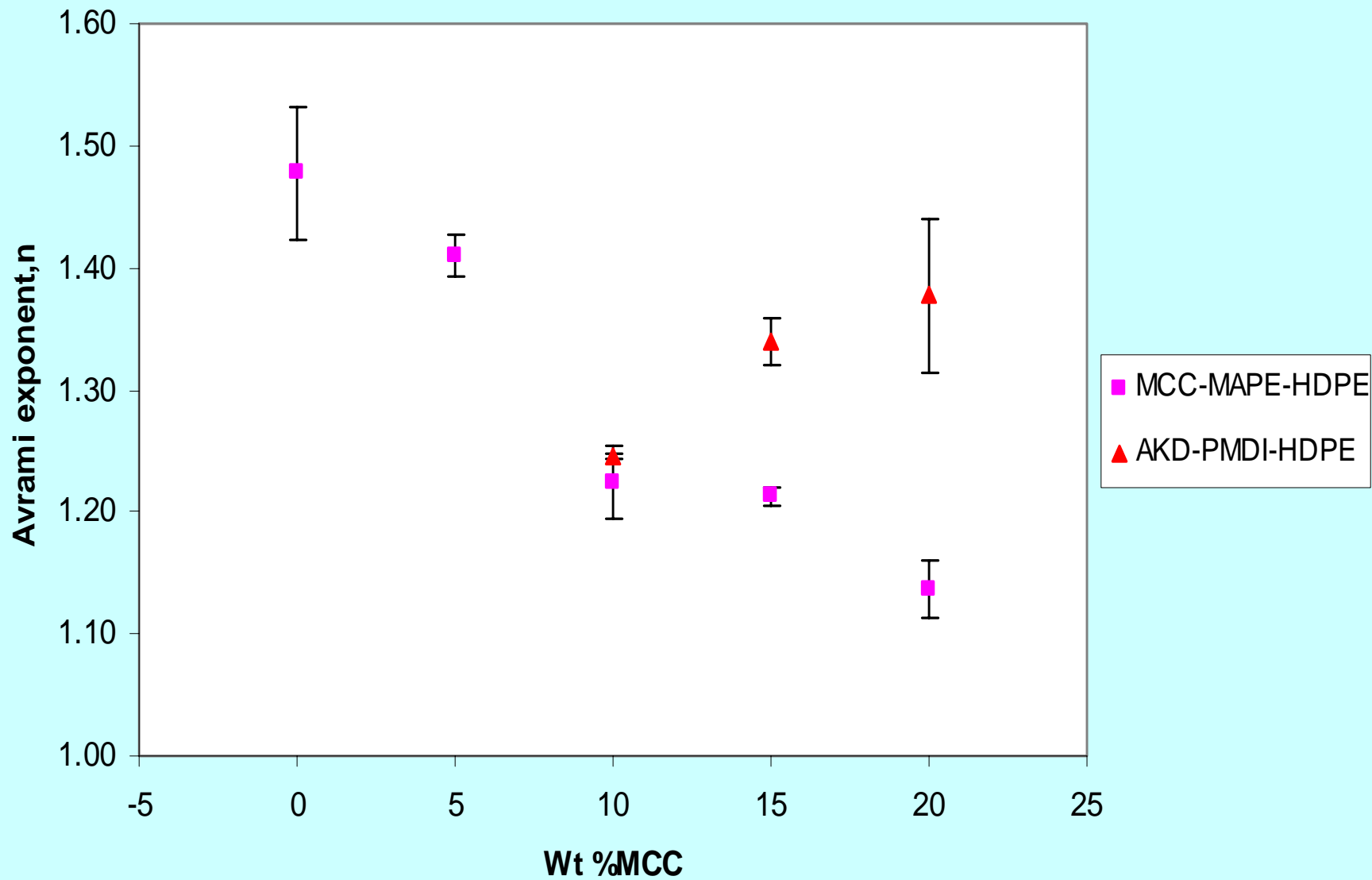
Percent Matrix Crystallinity



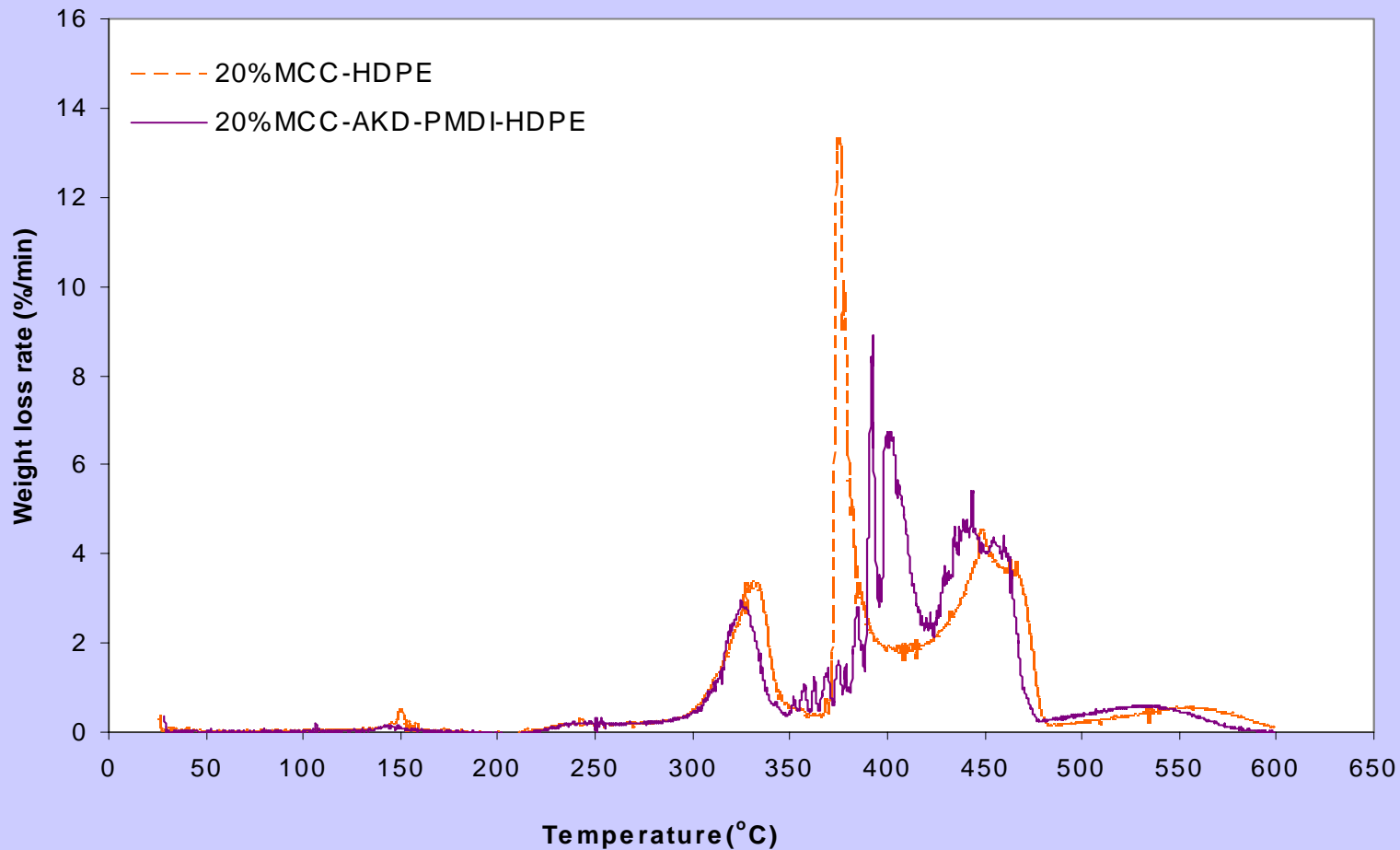
Activation Energy



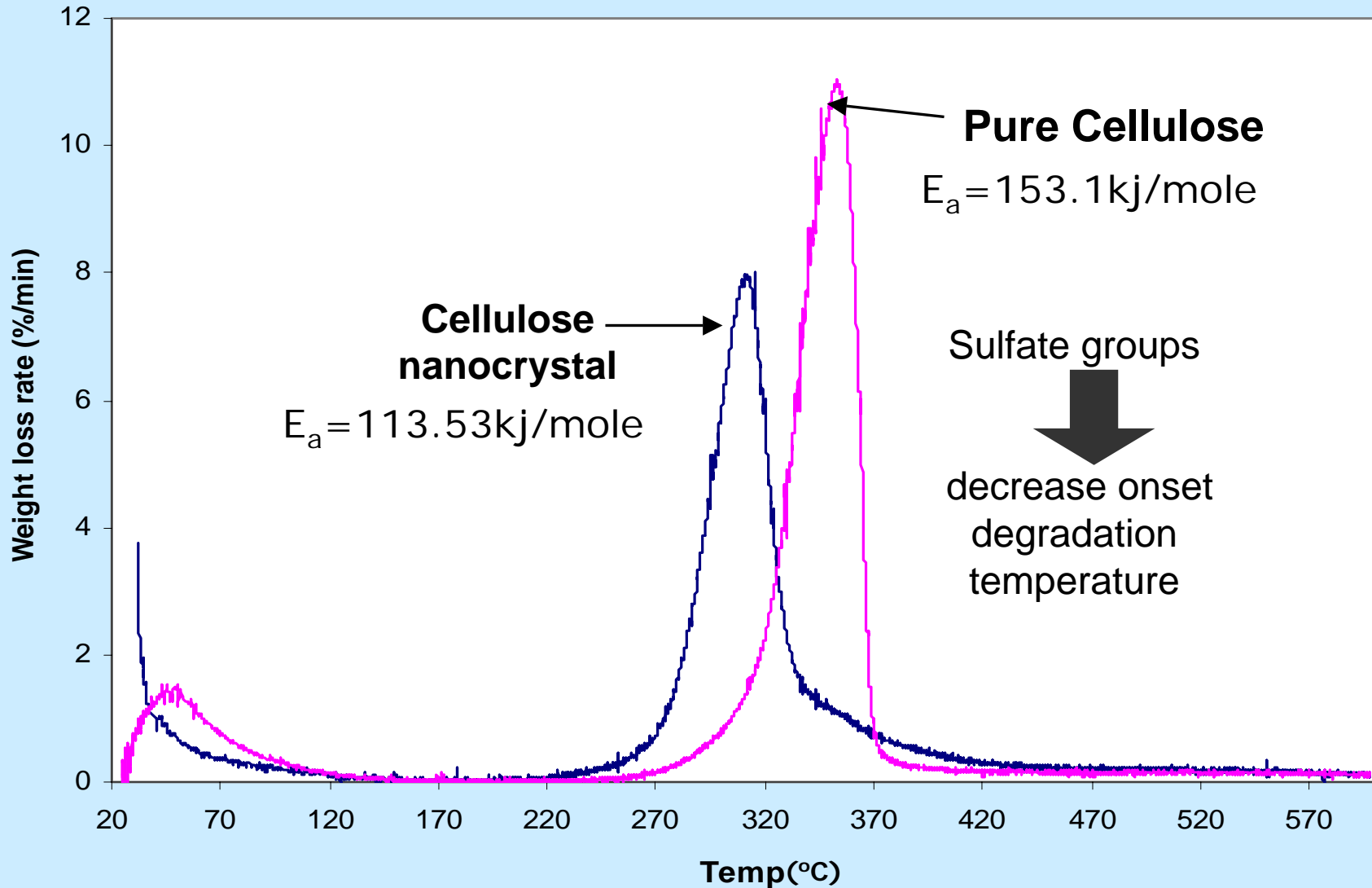
Avrami Exponent



Derivative Thermogravimetric (DTG) Curves



Derivative Thermogravimetric (DTG) Curves



Conclusions

- ⊕ **Coupling agents increase strength.**
- ⊕ **Fillers alter nucleation behavior**
- ⊕ **PMDI-AKD increases crystallinity.**
- ⊕ **PMDI-AKD changes the activation energy and peak crystallization temperature**
- ⊕ **Degradation behavior of the composite is not altered in the presence of compatibilizer.**
- ⊕ **Grafted sulfate groups decreases the activation energy and onset degradation temperature**
- ⊕ **The concept of compatibilizer systems can be extended to nanocomposites**

Acknowledgements

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⊕ Advisors

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